

# Indoor Energy Harvesting Enhancement: Pb-Free Perovskite Solar Cell with Nanograting Contact

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**Abstract** – Halide perovskite materials have spread in solar cells and photodetectors because of their excellent possibilities for tuning their absorption wavelengths, ease of fabrication, and low carbon footprint. However, their main drawbacks are related to their short device lifetime and stability problems in addition to limited efficiency at certain wavelength. For this reason, in this letter, we design a metasurface that can be integrated into a particularly long-life, stable, and sustainable perovskite solar cell with the aim of enhancing its performance under indoor conditions. The metasurface has been designed and numerically simulated to enhance the halide perovskite response at the typical emission wavelengths of indoor LEDs. Adjusting the response of these solar cells to those specific spectral ranges by metasurfaces may create novel energy harvesting devices.

**Keywords.** Perovskite solar cell, nanostructured grating, indoor energy harvesting, Pb-free, FDTD methods

## 1. Introduction

Halide perovskite solar cells (PSCs) are revolutionizing solar energy conversion due to their low-cost fabrication, high efficiencies (single-junction reach 26.7%, and tandem exceed 34%) [1, 2], and versatility for diverse applications including IoT and building integration [3, 4]. Their inherent properties, such as faster carrier dynamics and tunable bandgaps, are key to achieving up to 57% theoretical efficiency under indoor illumination, significantly exceeding the outdoor Shockley-Queisser limit of  $\sim 34\%$  [5, 6]. However, PSCs struggle with long-term stability due to crystallization defects, moisture, oxygen, and ionic migration [7]. Research currently focuses on developing stable, durable, and sustainable (Pb-free) materials and architectures to reach full deployment potential [8, 9, 10, 11, 12, 13]. One crucial strategy for enhancement is the incorporation of nanophotonic elements like metasurfaces [14]. These structures effectively manipulate light propagation to boost absorption at relevant wavelengths, increasing photocurrent, and enable functionalities such as color tunability and enhanced light trapping [15, 16, 17]. Nanograting structures are particularly promising for improved light management [18]. They introduce periodic patterns to increase light trapping and extend the optical path, which is crucial for thin-film devices where light absorption is limited

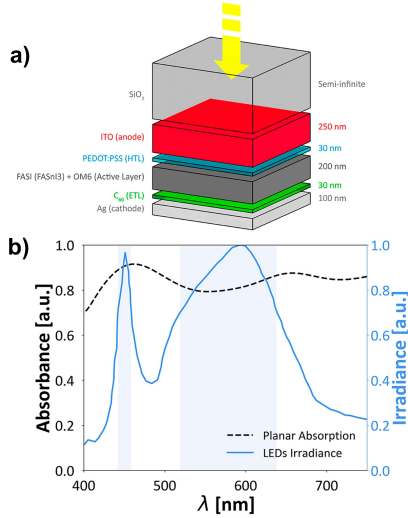
by layer thickness. This approach may either minimize Pb content or increase absorption in defective Sn-based PSCs. Optimized gratings support guided modes and resonances, increasing PCE without adding fabrication complexity [19]. Since poor positioning or refractive index mismatch can compromise performance [20], this study focuses on the numerical design of an optimal nanograting metasurface. Our goal is to improve the indoor performance of a Pb-free INAM-UJI PSC [21] by engineering a 1D diffraction grating within the hole transport layer (HTL) to increase absorbance at characteristic LED illumination peaks.

## 2. Methodology

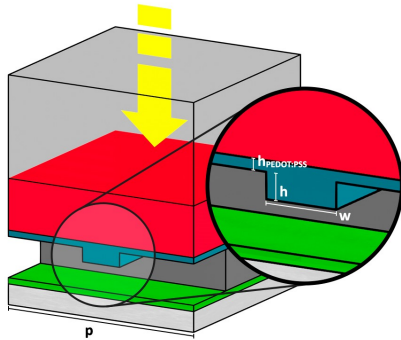
Numerical simulations were performed using the finite-difference time-domain (FDTD) method (Lumerical, Ansys ©). The unit cell reproduces the optically significant structure of the PSC shown in Fig. 1(a). Based on devices characterized in Ref. [21], the cell comprises a 200 nm active layer of FASI ( $FASnI_3$ ) modified with an OM6 organic additive to enhance stability. This layer is sandwiched between carrier extraction layers: a 30 nm hole transport layer (HTL) of PEDOT:PSS and a 30 nm electron transport layer (ETL) of  $C_{60}$ . A 250 nm indium tin oxide (ITO) anode and a 100 nm silver cathode serve as contacts, with a negligible BCP (bathocuproine) buffer layer and  $SiO_2$  encapsulation. As it is established in [22] the optical properties for

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54 PEDOT are essentially constant. The rest of the optical  
 55 parameters used as inputs come from both literature and  
 56 manufacturers, including the ones of the original planar  
 57 device [21]. Periodic boundary conditions (PBC) were  
 58 applied along the  $x$ - and  $y$ -axes, with perfectly matched  
 59 layers (PML) in the  $z$ -axis to simulate propagation. The  
 60 device was illuminated by a plane wave ( $z$ -propagating,  
 61  $x$ -polarized) with a spectrum derived from the average of  
 62 experimental indoor LED measurements taken at Carlos  
 63 III University of Madrid, as shown in Fig. 1(b).



**Figure 1:** (a) The planar structure of the perovskite solar cell that has been used in this work, including the most significant layers. In particular, an OM6-modified FASI is used as active layer with the aim of enhancing stability. (b) Spectral profile of the absorbance of the considered planar perovskite solar cell (left-axis) and the spectral emission of typical LED of indoor lighting systems (right axis).



**Figure 2:** Scheme of the proposed nanograting in the HTL surface to provide a larger light path control and enhance the effective absorbance of the PSC. Inset: detail of the structure with the most significant geometrical parameters.

64 The absorbed optical power in the halide perovskite  
 65 layer was calculated using electric field intensity ( $|E|^2$ )  
 66 and dielectric permittivity ( $\epsilon$ ) data obtained from 3D

67 FDTD monitors, same size as the perovskite active layer.  
 68 The absorbed power density is defined as:

$$P = -0.5\omega|E|^2 \text{Im}(\epsilon) \quad (1)$$

69 where  $\omega$  is the angular frequency of incident radiation  
 70 and  $\text{Im}(\epsilon)$  is the imaginary part of the perovskite di-  
 71 electric constant. Total absorption was determined by  
 72 integrating this optical power over the simulation vol-  
 73 ume. Figure 1(b) compares the Sn-OM6 cell absorption  
 74 with the average conventional LED lighting emission  
 75 spectrum. While the cell exhibits a broad absorption  
 76 band centered at 460 nm, absorption decreases signifi-  
 77 cantly in the higher wavelength region, highlighting a  
 78 clear opportunity for optimization.

### 79 3. Results and Discussion

80 We focus on the application of these devices in en-  
 81 ergy harvesting for indoor conditions. Therefore, we have  
 82 studied the most widely distributed luminaires: LEDs.  
 83 LED lighting implies a very different illumination from  
 84 the usual solar spectrum. While the first reaches a stan-  
 85 dard of  $100 \text{ mW}\cdot\text{cm}^{-2}$  (at AM1.5G), indoor lighting  
 86 only reaches a small fraction of it. Indeed, the spec-  
 87 trum is very different, with a usual peak around 450  
 88 nm due to the blue LED inside, and a spread emission  
 89 band around 600 nm due to the phosphor inside the  
 90 encapsulated luminaire. White LEDs can achieve combi-  
 91 nations of desired ambient lighting (cool or warm lights)  
 92 by balancing both emissions. To get a good overview  
 93 of real situations in which future applications will be  
 94 developed, we have measured a set of scenarios in actual  
 95 classrooms and laboratories of Carlos III University of  
 96 Madrid (UC3M), discarding those measurements close  
 97 to the windows during daylight hours (where the outdoor  
 98 lighting is at least one order of magnitude higher than  
 99 the indoor one). As was commented on, Fig. 1(b) de-  
 100 picts the average emission spectrum of the received light  
 101 on horizontal planes at user heights in those scenarios  
 102 (meanly, working tables or experimental setups).

103 After a prospective numerical work, the proposed  
 104 nanostructured grating is finally introduced in the HTL  
 105 layer (see Fig. 2) composed of ordered stripes with a  
 106 certain width in  $x$ -axis and a length exceeding the  
 107 unit cell size along  $y$ -axis to simulate an infinite bar.  
 108 Thus, the main geometric parameters of this structure  
 109 are the height ( $h$ ) and width ( $w$ ) of the grating, which  
 110 are optimized to maximize the absorption of the active  
 111 layer at the dominant wavelengths of indoor LEDs, as  
 112 shown in Fig. 1(b). Furthermore, the size of the unit cell  
 113 ( $p$ ) and the remaining thickness of the planar section  
 114 of the HTL ( $h_{\text{PEDOT:PSS}}$ ) are also included. For the  
 115 discretization, auto non-uniform mesh (mesh accuracy 4)  
 116 was selected. To improve the convergence of the results,  
 117 a refinement mesh in the grating was used with a 5 nm  
 118 size along the  $x$ -,  $y$ - and  $z$ -axis.

119 We parametrically investigated the nanograting's ge-  
 120 ometrical characteristics (like shape and size) to find the  
 121 optimal design for enhancing light absorption within  
 122 specific spectral ranges. To do this, we defined an

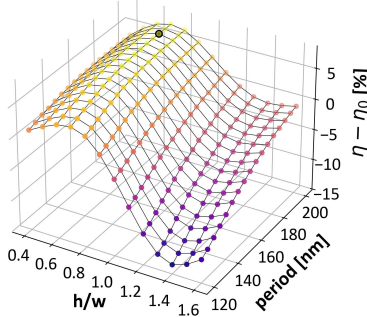
123 application-oriented absorption efficiency that specif-  
 124 ically weights the absorption of the cell by the actual  
 125 measured indoor LED light spectrum (as shown in Fig.  
 126 1(b)). This weighting, formalized in Equation 2, ensures  
 127 that the calculated efficiency reflects the true perfor-  
 128 mance of the device in indoor real-world conditions.

$$\eta = \frac{\int_{\lambda_0}^{\lambda_f} \text{Abs}(\lambda) \text{Irr}(\lambda) d\lambda}{\int_{\lambda_0}^{\lambda_f} \text{Irr}(\lambda) d\lambda} \quad (2)$$

129 Quantification of this absorption enhancement is ac-  
 130 complished through the introduction of a Figure of Merit  
 131 (FOM) formally defined as the differential absorption  
 132 efficiency (in percentage) as shown in Equation 3:

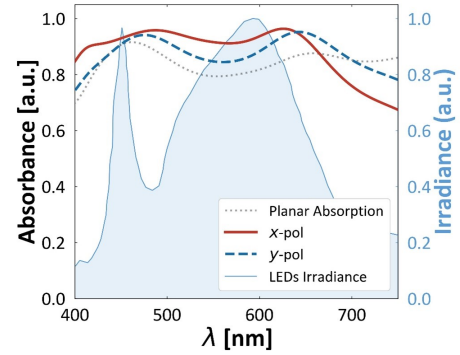
$$FOM = \frac{\eta - \eta_0}{\eta_0} \cdot 100 \quad (3)$$

133 being  $\eta$  and  $\eta_0$  the absorption efficiency with and without  
 134 the integration of the nanograting structure, respectively.



**Figure 3:** Differential absorption efficiency of the nanograting PSC as a function of both the ratio height/width of the stripes and the unit cell size or period. The width of the stripes has been fixed to a value of  $w = 100\text{nm}$ . The maximum (91.14 %) is shown at 190 nm period and a ratio of 0.7, represented against the reference (84.05 %).

135 Figure 3 shows a 3D plot of the percentage differential  
 136 absorption efficiency versus the geometric dimensions of  
 137 the structure. To facilitate the concise presentation and  
 138 clarification of the data, the derived results are graphi-  
 139 cally represented as a function of the following geometric  
 140 parameters: the aspect ratio of the stripes, defined as the  
 141 height-width ratio and the period of the modeled unit  
 142 cell (see Figure 2). The plot demonstrates a continuous  
 143 consistent response, showing that the magnitude of the  
 144 defined FOM -the differential absorption efficiency- is  
 145 positively correlated with the increasing period in the  
 146 studied interval (100 nm to 200 nm) except for a short  
 147 range close to 200 nm at low aspect ratio, while it first  
 148 increases, and then decreases with decreasing ratio. A  
 149 peak value of 7.09 percentage points constitutes the max-  
 150 imum observed, in a ratio of  $h/w = 0.7$  and a period of  
 151 190 nm. This optimum case, highlighted in the Figure,  
 152 particularly considers  $w = 100\text{nm}$ , being the width for  
 153 which the best result has been achieved. Moreover, it  
 154 is worth mentioning that this result is specific to the



**Figure 4:** Active layer absorbance for the planar and opti-  
 mized structures is presented as a function of incident  
 wavelength ( $\lambda$ ). The characterized LED emission spectrum  
 is superimposed to assess the resulting performance enhance-  
 ment under the specified illumination.

155 active layer, indicating a potential similar improvement  
 156 in the generated photocurrent.

157 The active layer absorbance spectrum for both the  
 158 planar reference structure and the proposed nanograting  
 159 structure integrated into the HTL is shown in Figure  
 160 4. Near-field profiles obtained resolve a field redistri-  
 161 bution around the nanograting that increases the light  
 162 intensity in the active layer, and thus, absorption. The  
 163 nanograting primarily improves the overall absorbance  
 164 for incident wavelengths ( $\lambda$ ) less than 675 nm, although  
 165 it causes a degradation in performance for  $\lambda > 675$   
 166 nm. Crucially, the performance of the PSC is signifi-  
 167 cantly improved within the specific spectral region of  
 168 interest under LED illumination, particularly due to a  
 169 pronounced increase in the absorption in the active layer  
 170 within the  $\lambda$  interval of 520 nm to 620 nm. This region  
 171 directly aligns with a major LED emission peak at  $\sim 600$   
 172 nm. Although x-polarized light shows a better response,  
 173 y-polarized one also slightly enhances the planar case  
 174 around similar wavelength intervals, with an increment  
 175 of 4.59 percentage points. Thus, whenever the cell is un-  
 176 der indoor illumination, the absorption will be improved,  
 177 also showing polarization sensitivity. This enhancement  
 178 is characterized by a blue-shift in the peak absorbance  
 179 from  $\sim 650$  nm in the planar structure to  $\sim 615$  nm in  
 180 the nanostructure, achieving a closer spectral match to  
 181 the  $\sim 600$  nm LED peak irradiance. Furthermore, the  
 182 proposed PSC exhibits a slight but beneficial increase  
 183 in absorbance in the spectral region corresponding to  
 184 the secondary LED emission peak ( $\sim 450$  nm), which  
 185 also significantly increases overall performance in that  
 186 region. Thus, this nanostructure effectively enhances the  
 187 overall absorbance in the spectral range from 400 nm to  
 188 650 nm, relative to the planar structure, while absorp-  
 189 tion decreases for  $\lambda > 650$  nm, signifying the successful  
 190 achievement of spectral shape matching between the  
 191 active layer absorbance profile and the LED irradiance  
 192 spectrum within the critical operating interval. Other  
 193 2D structures have been tested, but as their results are  
 194 close to the ones exposed here, significant limitations  
 195 due to their difficult nanofabrication and integration into

196 device architectures may reduce the feasibility of using  
197 them to improve these PSCs for indoor applications.

## 198 4. Conclusion

199 In this work, we first established a magnitude of  
200 interest that allows us to pinpoint the performance en-  
201 hancement of a novel Pb-free Sn-based perovskite solar  
202 cell in an indoor room. We weigh the spectral absorbance  
203 of the cell by an irradiance spectrum, which is the aver-  
204 age of a weighed efficiency, which is dependent on the  
205 lighting conditions around the cell. This leads to a sim-  
206 ple figure of merit to understand the level of theoretical  
207 enhancement, by comparing the planar cell efficiency,  
208 taken as the reference case, with that of the cell with  
209 the proposed nanograting, as the improved one. **To iso-**  
210 **late the optical impact of the nanostructure, our model**  
211 **assumes constant electrical parameters, acknowledging**  
212 **that the electronic challenges of increased interfacial area**  
213 **are effectively addressed in experimental settings via sur-**  
214 **face passivation layers. Moreover, such nanogratings can**  
215 **facilitate improved carrier extraction by reducing the**  
216 **transport distance to the contacts, provided that con-**  
217 **formal film deposition is achieved.**

218 We have explored several geometries, achieving the  
219 best results with the use of 1D grating simulated in the  
220 device structure that was manufactured in one of our pre-  
221 vious works. An optimized result is obtained at a geomet-  
222 rical form factor of the grid of  $h/w = 0.7$  and a period of  
223 190 nm. **An average of 5.84% optical enhancement (with**  
224 **a maximum of 7.09% under x-polarization) confirms the**  
225 **feasibility of using nanograting-based Pb-free cells for**  
226 **indoor energy harvesting. In line with literature [23],**  
227 **our results suggest a proportional boost in electron-hole**  
228 **generation and short-circuit current, provided carrier ex-**  
229 **traction remains efficient.** These results allow exploring  
230 Internet of Things applications where these cells can be  
231 used as energy harvesting photovoltaic devices, recycling  
232 ambient light to create fully autonomous wireless (but  
233 cloud-connected) systems.

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## 245 Conflicts of interest

246 The authors have nothing to disclose.

## 247 Data availability statement

248 There is an associated dataset available at:  
249 <https://doi.org/10.21950/J69M96>.

## 250 Author contribution statement

251 Conceptualization, B.G-C, A.B., I.M., R.V., and A.G-M;  
252 Methodology, R.V., B.G-C, A.B., E.L-F and D.S.; Software, D.S.;

254 Data Curation, D.S., R.V.; Writing – Original Draft Preparation, R.V.,  
255 B.G-C and D.S.; Writing – Review Editing, Visualization, all authors;  
256 Supervision, Project Administration, Funding Acquisition, R.V.

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